



Engineering

tec instruct LLC
4111 164th St SW
Unit 51
Lynnwood, WA 98087
Phone (206) 553 9076
rheimisch@yahoo.com

STRUCTURAL DESIGN

| | |
|----------------------------|--|
| Owner: | James & Brooke Aldrich |
| Project: | 7448 W Mercer Way Mercer Island, WA 98040 |
| Description: | Addition and Alteration |
| Building Codes: | IBC/IRC 2021 ASCE 7-16 |
| Structural Design/ EOR: | Roland Heimisch, P. E. Lic # 42479 |
| Date | 04/28/2025 |





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1. LATERAL DESIGN

Project: 7448 W Mercer Way, Mercer Island, 98040

1.1 Seismic Design

| | | | | |
|-----------------|--------------------------------------|-----------------|---|---------------------------------|
| Criteria | Basic Seismic-Force-Resisting System | | | Diaphragms / Shear Walls |
| | Medium Building Height | H | = | 15 ft |
| | Seismic Use Group | | | II |
| | Importance Factor | I _e | = | 1.0 |
| | Site Class | | | D |
| | Seismic Design Category | | | D |
| | Response Factor | R | = | 6.5 (light frame wood building) |
| | Mapped Acceleration | S _s | = | 1.65 |
| | | S ₁ | = | 0.63 |
| | Design Acceleration | SD _s | = | 1.16 |
| | | SD ₁ | = | NA |
| | Seismic Response Coefficient | C _s | = | SD _s / (R/I) |
| | | | = | 1.16 / (6.5/1.0) = 0.18 |

Building Weight

$$W = 15 \text{ psf} \times 2,600 \text{ sqft} = 39,000 \text{ lbs}$$

Base Shear $V_{\text{Base}} = C_s \times W = 0.18 \times 39,000 = 7,000 \text{ lbs}$

Design Shear: To convert from strength level to ASD, Base Shear is multiplied by 0.7

$$V_{\text{Design}} = 0.7 \times 7,000 = 4,900, \text{ say } 5,000 \text{ lbs}$$

Seismic Load per Grid: Grids 6 & B $0.25 \times 5,000 = 1,250 \text{ lbs}$

Grids 2 & C $0.50 \times 5,000 = 2,500 \text{ lbs}$

REPORT SUMMARY

Site Information

| | |
|----------------|---|
| Address: | 7448 W Mercer Way, Mercer Island, Washington, 98040 |
| Elevation: | 241 ft (NAVD 88) |
| Lat: | 47.535985 |
| Long: | -122.238503 |
| Standard: | ASCE/SEI 7-22 |
| Risk Category: | II |
| Soil Class: | D - Stiff Soil |

Seismic Data

| | |
|-------------------------|--|
| S_s | 1.65 |
| S_1 | 0.63 |
| S_{MS} | 1.74 |
| S_{M1} | 1.29 |
| S_{DS} | 1.16 |
| S_{D1} | 0.86 |
| T_L | 6 |
| PGA_M | 0.74 |
| V_{S30} | 260 |
| Seismic Design Category | D |
| Note | Where values of the multi-period 5%-damped MCER response spectrum are not available from the USGS Seismic Design Geodatabase, the design response spectrum shall be permitted to be determined in accordance with Section 11.4.5.2 |

Project: 7448 W Mercer Way, Mercer Island, 98040

1.2 Wind Design

Directional Procedure, Part 2 (simplified method) per ASCE 7-22

| | | |
|-------------------------|--|----------|
| Design Criteria: | Enclosed Simple Diaphragm Building | |
| | Risk Category II | |
| | Basic Wind Speed per Table 26.5-1A | 110 MpH |
| | Directionality Factor K_d | 0.85 |
| | Exposure Category | B |
| | Wind Speed up factor K_{zt} | 1.0 |
| | Enclosure Classification | enclosed |
| | Net pressure at top of wall p_h , Table 27.6-1 | 17.5 psf |
| | (conservatively also used for bottom of wall) | |

As the shear wall design is performed for ASD, the load is multiplied with 0.7

| | | |
|-----------------------|-------------------|-------------------|
| Applied wind pressure | 0.7×17.5 | 12.25, say 13 psf |
|-----------------------|-------------------|-------------------|

Uniform wind load on diaphragms

| | | | | |
|-----------------|-----|---------|---|---------|
| w/ trib h 10 ft | w = | 10 x 13 | = | 130 plf |
|-----------------|-----|---------|---|---------|

| | | | | |
|-----------------------------|------------|----------------------------|---|-----------|
| Wind loads per grid: | Grid 6 | $0.5 \times 20 \times 130$ | = | 1,300 lbs |
| | Grid 2 | $0.5 \times 65 \times 130$ | = | 4,225 lbs |
| | Grid A & C | $0.5 \times 68 \times 130$ | = | 4,420 lbs |
| | Grid B | $0.5 \times 28 \times 130$ | = | 1,820 lbs |

Grids A and 5 are existing to remain

Shear Wall Types

| SW type | OSB | Nails | Nails edge @ (in o.c.) | Nails field @ (in o.c.) | Boundary Member | Seismic list x .94 (to adjust for HF) | Wind Anchor x 1.4 Bolt 5/8" @ (in o.c.) |
|---------|----------|-------|------------------------|-------------------------|-----------------|---------------------------------------|---|
| P1-6 | 7/16" | 8d | 6" | 12" | 2x | 225 | 315 48" |
| P1-3 | 7/16" | 8d | 3" | 12" | 3x | 425 | 590 30" |
| Roof | 7/16" | 8d | 6" | 12" | 2x | 226 | 316 |
| Floor | 3/4" CDX | 10d | 6" | 12" | 2x | 300 | 420 |

Holdowns

| Callout | HD | All T (lbs) | Wood Member | Bolt dia | Embedment w/ Epoxy SET-G3 |
|---------|------|-------------|-------------|----------|---------------------------|
| 1 | HDU2 | 2215 | (2) 2x | 5/8" | 7" |
| 2 | HDU4 | 3285 | (2) 2x | 5/8" | 9" |

Wind loads

| Shear design | | Overturning | | | | | | | | | | | | | | |
|--|---------------|---------------------|-----------------------|-------------|-------|--------|--------|------------------|--------------|------------------|------------------|----------------------|---------------|----------------|-----------------|--|
| Grid | Shear V (lbs) | Length total L (ft) | Shear uniform v (plf) | SW Type | Panel | L (ft) | h (ft) | Aspect Ratio k/L | M ot (lb-ft) | Wall trib.H (ft) | R/FI trib.L (ft) | M res Restr. (lb-ft) | M tot (lb-ft) | Uplift T (lbs) | HW | |
| 6 | 1300 | 28.0 | 46 | P1-6 | 6-1 p | 28.00 | 8 | 0.29 | 10400 | 8 | 2 | 23100 | -12700 | -454 | not reqd | |
| 2 | 4225 | 17.5 | 241 | P1-6 | 2-1 | 4.00 | 8 | 2 | 7726 | 8 | 6 | 588 | 7138 | 1784 | HDU2 | |
| | | | | | 2-2 | 8.00 | 8 | 1 | 15451 | 8 | 6 | 2520 | 12931 | 1616 | HDU2 | |
| | | | | | 2-3 | 5.50 | 8 | 1.45 | 10623 | 8 | 6 | 1155 | 9468 | 1721 | HDU2 | |
| Sheathing, nailing pattern, and holdowns in Grid 2 to be verified | | | | | | | | | | | | | | | | |
| A | 4420 | 35.0 | 126 | P1-6 | A-1 | 2.50 | 8 | 3.2 | 2526 | 8 | 14 | 330 | 2196 | 878 | HDU2 | |
| Existing grid, to be verified | | | | | | | | | | | | | | | | |
| B | 1820 | 5.0 | 364 | P1-3 | B-1 | 2.50 | 8 | 3.2 | 7280 | 8 | 14 | 330 | 6950 | 2780 | HDU4 | |
| | | | | | B-2 | 2.50 | 8 | 3.2 | 7280 | 8 | 14 | 330 | 6950 | 2780 | HDU4 | |
| C | 4420 | 20.0 | 221 | P1-6 | C-1 | 20.00 | 8 | 0.4 | 35360 | 8 | 14 | 25740 | 9620 | 481 | HDU2 | |

Bold indicates that wind governs

p perforated panel

| Panel | Unit Shear v (plf) | h op % | Σ Li (ft) | L total (ft) | Sheathing ΣLi / L % | Co | q' (plf) | Nailing |
|-------|--------------------|--------|-----------|--------------|---------------------|------|----------|---------|
| 6-1 | 46 | 5h/6 | 16 | 28 | 57 | 0.61 | 132 | P1-6 |

Wind loads

| Shear design | | Overturning | | | | | | | | | | | | | |
|--|---------------|---------------------|-----------------------|-------------|-------|--------|--------|------------------|--------------|------------------|------------------|----------------------|---------------|----------------|----------|
| Grid | Shear V (lbs) | Length total L (ft) | Shear uniform v (plf) | SW Type | Panel | L (ft) | h (ft) | Aspect Ratio k/L | M ot (lb-ft) | Wall trib.H (ft) | R/FI trib.L (ft) | M res Restr. (lb-ft) | M tot (lb-ft) | Uplift T (lbs) | HW |
| 6 | 1250 | 28.0 | 45 | P1-6 | 6-1 p | 28.00 | 8 | 0.29 | 10000 | 8 | 2 | 23100 | -13100 | -468 | not reqd |
| 2 | 2500 | 17.5 | 143 | P1-6 | 2-1 | 4.00 | 8 | 2 | 4571 | 8 | 6 | 588 | 3983 | 996 | HDU2 |
| | | | | | 2-2 | 8.00 | 8 | 1 | 9143 | 8 | 6 | 2520 | 6623 | 828 | HDU2 |
| | | | | | 2-3 | 5.50 | 8 | 1.45 | 6286 | 8 | 6 | 1155 | 5131 | 933 | HDU2 |
| Sheathing, nailing pattern, and holdowns in Grid 2 to be verified | | | | | | | | | | | | | | | |
| A | 2500 | 35.0 | 71 | P1-6 | A-1 | 2.50 | 8 | 3.2 | 1429 | 8 | 14 | 330 | 1099 | 439 | HDU2 |
| Existing grid, to be verified | | | | | | | | | | | | | | | |
| B | 1250 | 5.0 | 250 | P1-3 | B-1 | 2.50 | 8 | 3.2 | 5000 | 8 | 14 | 330 | 4670 | 1868 | HDU2 |
| | | | | | B-2 | 2.50 | 8 | 3.2 | 5000 | 8 | 14 | 330 | 4670 | 1868 | HDU2 |
| C | 2500 | 20.0 | 125 | P1-6 | C-1 | 20.00 | 8 | 0.4 | 20000 | 8 | 14 | 25740 | -5740 | -287 | not reqd |

Bold indicates that wind governs

p perforated panel

| Panel | Unit Shear v (plf) | h op % | Σ Li (ft) | L total (ft) | Sheathing ΣLi / L % | Co | q' (plf) | Nailing |
|-------|--------------------|--------|-----------|--------------|---------------------|------|----------|---------|
| 6-1 | 63 | 5h/6 | 16 | 28 | 57 | 0.61 | 181 | P1-6 |



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rheimisch@yahoo.com

2. GRAVITY DESIGN

Project: 7448 W Mercer Way, Mercder Island, WA 98040

2.1 Design Criteria

| | | | |
|-------------------|---------------------------------------|---------------------------------------|-------------------------|
| Dead Loads | Roof | Coating/Waterproofing | 2.0 |
| | | Sheathing OSB/Plywood 15/32" | 2.0 |
| | | Trusses / Framing | 3.0 |
| | | Insulation R-38 | 1.2 |
| | | Gypsum Board 5/8" | 2.8 |
| | | Miscellaneous (Sprinkler, HVAC etc) | 1.5 |
| | | Total | 12.5, say 15 psf |
| | Floors Living | Finished Floor (carpet) | 1.0 |
| | | Sheathing OSB/Plywood 3/4" | 2.5 |
| | | Floor Joists / TJIs | 2.5 |
| | | Insulation R-11 | 1.0 |
| | | Gypsum Board 5/8" | 2.8 |
| | | Miscellaneous (Sprinkler, HVAC etc) | 1.5 |
| | | Total | 11.3, say 15 psf |
| | Decks/Balconies | Decking | 3.0 |
| | | Floor Joists / TJIs | 2.5 |
| | | Miscellaneous (Railing/Waterproofing) | 1.5 |
| | | Total | 7.0 say 10 psf |
| | Ext. Walls | Siding | 3.0 |
| | | Sheathing 15/32" OSB/Plywood | 2.0 |
| | | 2x6" Studs @ 16" o.c. | 1.5 |
| | | Insulation R-21 | 0.6 |
| | | Gypsum Board 5/8" | 2.8 |
| | | Total | 9.9, say 10 psf |
| | Int. Walls | 2x4" Studs @ 16" o.c. | 1.5 |
| | | Gypsum Board (2 sides) 5/8" | 5.6 |
| | | Total | 7.1, say 8 psf |
| Live Loads | Roof | 25 psf | |
| | Living areas | 40 psf | |
| | Decks/Balconies | 60 psf | |
| Snow Load | Snow Ground Load | 25 psf | |
| | Snow Roof Load (no reduction applied) | 25 psf | |

Project: 7448 W Mercer Way, Mercder Island, WA 98040

2.2 Key List

Roof Level

- Key No. 1.1 **Manufactured Scissored Trusses, @ 24" o.c.**
- Key No. 1.2 **Manufactured Common Trusses, @ 24" o.c.**
- Key No. 1.3 **Glulam WS, 24F-1.8E, 5-1/2x9-1/2"**
- Key No. 1.4 **Post, HF No. 2, 6x6", P.T.**
- Key No. 1.5 **Glulam WS, 24F-1.8E, 5-1/2x13-1/2"**
- Key No. 1.6 **Header, DF No. 2, 4x6"**

Floor Level

- Key No. 2.1 **Floor Joist, F No. 2, 2x10", @ 16" o.c.**
- Key No. 2.2 **Beam, DF No. 2, 6x10"**
- Key No. 2.3 **Continuous Footing, fc = 2,500 psi, 16x8"**
- Key No. 2.4 **Spread Footing, fc = 2,500 psi, 24x24x8"**

Project: 7448 W Mercer Way, Mercder Island, WA 98040

2.3 Roof

Key No. 1.1 Manufactured Scissored Trusses, @ 24" o.c.

| | | | |
|------------------|-------|---|--------|
| Span: | max L | = | 28 ft |
| Load: | DL | = | 15 psf |
| | SL | = | 25 psf |
| Per manufacturer | | | |

Key No. 1.2 Manufactured Common Trusses, @ 24" o.c.

| | | | |
|------------------|-------|---|--------|
| Span: | max L | = | 16 ft |
| Load: | DL | = | 15 psf |
| | SL | = | 25 psf |
| Per manufacturer | | | |

Key No. 1.3 Glulam WS, 24F-1.8E, 5-1/2x9-1/2"

| | | | |
|-------|-------------------|---|---------|
| Span: | L | = | 16 ft |
| Load: | roof w/ trib 8 ft | | |
| | DL 8 x 15 | = | 120 plf |
| | SL 8 x 25 | = | 200 plf |

For calculation see design sheets

Key No. 1.4 Post, HF No. 2, 6x6", P.T.

| | | | |
|---------|------------------------|---|-----------|
| height: | H | = | 8 ft |
| Load: | reaction from beam 1.3 | | |
| | PDL | = | 965 lbs |
| | PSL | = | 1,610 lbs |

Per inspection

Key No. 1.5 Glulam WS, 24F-1.8E, 5-1/2x13-1/2"

| | | | |
|-------|--------------------|---|---------|
| Span: | L | = | 16 ft |
| Load: | roof w/ trib 22 ft | | |
| | DL 22 x 15 | = | 330 plf |
| | SL 22 x 25 | = | 550 plf |

For calculation see design sheets

Key No. 1.6 Header, DF No. 2, 4x6"

| | | | |
|-------|-------------------|---|--------|
| Span: | L | = | 6 ft |
| Load: | roof w/ trib 2 ft | | |
| | DL 2 x 15 | = | 30 plf |
| | SL 2 x 25 | = | 50 plf |

For calculation see design sheets

Project: 7448 W Mercer Way, Mercder Island, WA 98040

2.4 Floor Level and Foundation

Key No. 2.1 Floor Joist, F No. 2, 2x10", @ 16" o.c.

| | | | |
|-----------------------------------|----|---|--------|
| Span: | L | = | 10 ft |
| Loads: | DL | = | 15 psf |
| | LL | = | 40 psf |
| For calculation see design sheets | | | |

Key No. 2.2 Beam, DF No. 2, 6x10"

| | | | |
|-----------------------------------|---------------------|---------|-----------|
| Span: | L | = | 9 ft |
| Load: | floor w/ trib 10 ft | | |
| | DL | 10 x 15 | = 150 plf |
| | LL | 10 x 40 | = 400 plf |
| For calculation see design sheets | | | |

Key No. 2.3 Continuous Footing, $f_c = 2,500$ psi, 16x8"

Dimensions per prescriptive requirements
 Reinforcement: (2) rebars # 4 longitudinal
 Transverse #3 @ 18" o.c.

Key No. 2.4 Spread Footing, $f_c = 2,500$ psi, 24x24x8"

| | | | |
|---------------|---|------------------|---------------------|
| Load | reaction from (2x) beam 2.2 (governs over post 1.4) | | |
| | P | $2 \times 2,500$ | = 5,000 lbs |
| Soil pressure | | $5,000 / 4$ | = 1,250 psf < 1,500 |
| Rebars | # 4 @ 6" o.c. both directions | | |



7448 W Mercer Island
Mercer Island, WA 98040
1_3 Beam
Apr. 23, 2025 14:54

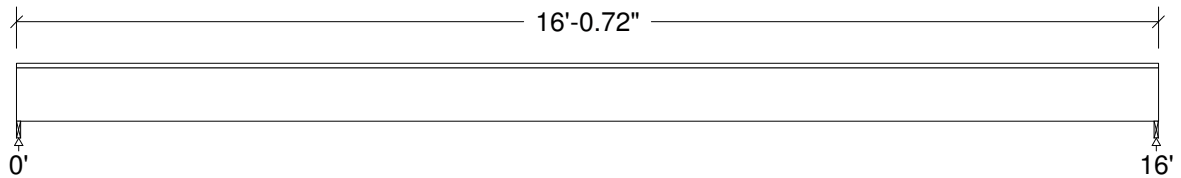
Design Check Calculation Sheet

WoodWorks Sizer 2023

Loads:

| Load | Type | Distribution | Pat-tern | Location [ft] | | Magnitude | | Unit |
|------|------|--------------|----------|---------------|-----|-----------|-----|------|
| | | | | Start | End | Start | End | |
| DL | Dead | Full UDL | | | | 120.0 | | plf |
| SL | Snow | Full UDL | | | | 200.0 | | plf |

Maximum Reactions (lbs), Bearing Capacities (lbs) and Bearing Lengths (in) :



| | | | |
|-------------|------|--|------|
| Unfactored: | | | |
| Dead | 964 | | 964 |
| Snow | 1606 | | 1606 |
| Factored: | | | |
| Total | 2570 | | 2570 |
| Bearing: | | | |
| Capacity | | | |
| Beam | 2570 | | 2570 |
| Support | 2639 | | 2639 |
| Des ratio | | | |
| Beam | 1.00 | | 1.00 |
| Support | 0.97 | | 0.97 |
| Load comb | #2 | | #2 |
| Length | 0.72 | | 0.72 |
| Min req'd | 0.72 | | 0.72 |
| Cb | 1.00 | | 1.00 |
| Cb min | 1.00 | | 1.00 |
| Cb support | 1.07 | | 1.07 |
| Fcp sup | 625 | | 625 |

Glulam-Unbalan., West Species, 24F-1.8E WS, 5-1/2"x9"

Supports: All - Timber-soft Beam, D.Fir-L (N) No.2

Total length: 16'-0.75"; Clear span: 15'-11.25"; Volume = 5.5 cu.ft.; 6 laminations, 5-1/2" maximum width,
Lateral support: top = continuous, bottom = at supports;

This section PASSES the design code check.

Analysis vs. Allowable Stress and Deflection using NDS 2018 :

| Criterion | Analysis Value | Design Value | Unit | Analysis/Design |
|--------------|----------------|----------------|------|-------------------|
| Shear | $f_v = 70$ | $F_v' = 305$ | psi | $f_v/F_v' = 0.23$ |
| Bending (+) | $f_b = 1655$ | $F_b' = 2760$ | psi | $f_b/F_b' = 0.60$ |
| Live Defl'n | $0.49 = L/391$ | $0.53 = L/360$ | in | 0.92 |
| Total Defl'n | $0.78 = L/244$ | $1.07 = L/180$ | in | 0.74 |

Additional Data:

| FACTORS: | F/E (psi) | CD | CM | Ct | CL | CV | Cfu | Cr | Cfrt | Notes | Cvr | LC# |
|---------------------|--------------|------|------|------|-------|-------|-----|----|------|-------|------|-----|
| Fv' | 265 | 1.15 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 1.00 | 2 |
| Fb'+ | 2400 | 1.15 | 1.00 | 1.00 | 1.000 | 1.000 | - | - | 1.00 | 1.00 | - | 2 |
| Fcp' | 650 | - | 1.00 | 1.00 | - | - | - | - | 1.00 | - | - | - |
| E' | 1.8 million | | 1.00 | 1.00 | - | - | - | - | 1.00 | - | - | 2 |
| E _{miny} ' | 0.85 million | | 1.00 | 1.00 | - | - | - | - | 1.00 | - | - | 2 |

CRITICAL LOAD COMBINATIONS:

Shear : LC #2 = D + S
 Bending (+): LC #2 = D + S
 Deflection: LC #2 = D + S (live)
 LC #2 = D + S (total)
 Bearing : Support 1 - LC #2 = D + S
 Support 2 - LC #2 = D + S

D=dead S=snow

All LC's are listed in the Analysis output

Load Patterns: s=S/2, X=L+S or L+Lr, _=no pattern load in this span

Load combinations: ASD Basic from ASCE 7-16 2.4

CALCULATIONS:

V max = 2560, V design = 2310 (NDS 3.4.3.1(a)) lbs; M(+) = 10240 lbs-ft

EI = 601.42e06 lb-in²

"Live" deflection is due to all non-dead loads (live, wind, snow...)

Total deflection = 1.00 permanent + "live"

Design Notes:

1. Analysis and design are in accordance with the ICC International Building Code (IBC 2021) and the National Design Specification (NDS 2018), using Allowable Stress Design (ASD). Design values are from the NDS Supplement.
2. Please verify that the default deflection limits are appropriate for your application.
3. Glulam design values are for materials conforming to ANSI 117-2015 and manufactured in accordance with ANSI A190.1-2012
4. GLULAM: bxd = actual breadth x actual depth.
5. Glulam Beams shall be laterally supported according to the provisions of NDS Clause 3.3.3.
6. GLULAM: bearing length based on smaller of Fcp(tension), Fcp(comp'n).



7448 W Mercer Island
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1_5 GLB
Apr. 23, 2025 15:30

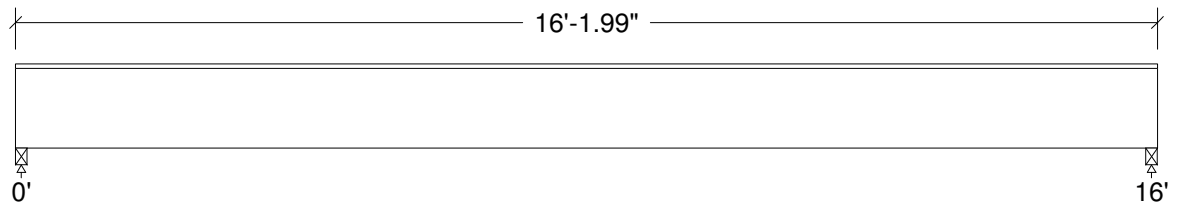
Design Check Calculation Sheet

WoodWorks Sizer 2023

Loads:

| Load | Type | Distribution | Pat-tern | Location [ft] | | Magnitude | | Unit |
|------|------|--------------|----------|---------------|-----|-----------|-----|------|
| | | | | Start | End | Start | End | |
| DL | Dead | Full UDL | | | | 330.0 | | plf |
| SL | Snow | Full UDL | | | | 550.0 | | plf |

Maximum Reactions (lbs), Bearing Capacities (lbs) and Bearing Lengths (in) :



| | | | |
|-------------|------|--|------|
| Unfactored: | | | |
| Dead | 2667 | | 2667 |
| Snow | 4446 | | 4446 |
| Factored: | | | |
| Total | 7113 | | 7113 |
| Bearing: | | | |
| Capacity | | | |
| Beam | 7113 | | 7113 |
| Support | 7306 | | 7306 |
| Des ratio | | | |
| Beam | 1.00 | | 1.00 |
| Support | 0.97 | | 0.97 |
| Load comb | #2 | | #2 |
| Length | 1.99 | | 1.99 |
| Min req'd | 1.99 | | 1.99 |
| Cb | 1.00 | | 1.00 |
| Cb min | 1.00 | | 1.00 |
| Cb support | 1.07 | | 1.07 |
| Fcp sup | 625 | | 625 |

Glulam-Unbalan., West Species, 24F-1.8E WS, 5-1/2"x13-1/2"

Supports: All - Timber-soft Beam, D.Fir-L (N) No.2

Total length: 16'-2.0"; Clear span: 15'-10"; Volume = 8.3 cu.ft.; 9 laminations, 5-1/2" maximum width,

Lateral support: top = continuous, bottom = at supports;

This section PASSES the design code check.

Analysis vs. Allowable Stress and Deflection using NDS 2018 :

| Criterion | Analysis Value | Design Value | Unit | Analysis/Design |
|--------------|----------------|----------------|------|-------------------|
| Shear | $f_v = 121$ | $F_v' = 305$ | psi | $f_v/F_v' = 0.40$ |
| Bending (+) | $f_b = 2023$ | $F_b' = 2760$ | psi | $f_b/F_b' = 0.73$ |
| Live Defl'n | $0.40 = L/480$ | $0.53 = L/360$ | in | 0.75 |
| Total Defl'n | $0.64 = L/300$ | $1.07 = L/180$ | in | 0.60 |

Additional Data:

| FACTORS: | F/E (psi) | CD | CM | Ct | CL | CV | Cfu | Cr | Cfrt | Notes | Cvr | LC# |
|---------------------|--------------|------|------|------|-------|-------|-----|----|------|-------|------|-----|
| Fv' | 265 | 1.15 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 1.00 | 2 |
| Fb'+ | 2400 | 1.15 | 1.00 | 1.00 | 1.000 | 1.000 | - | - | 1.00 | 1.00 | - | 2 |
| Fcp' | 650 | - | 1.00 | 1.00 | - | - | - | - | 1.00 | - | - | - |
| E' | 1.8 million | | 1.00 | 1.00 | - | - | - | - | 1.00 | - | - | 2 |
| E _{miny} ' | 0.85 million | | 1.00 | 1.00 | - | - | - | - | 1.00 | - | - | 2 |

CRITICAL LOAD COMBINATIONS:

Shear : LC #2 = D + S
 Bending (+): LC #2 = D + S
 Deflection: LC #2 = D + S (live)
 LC #2 = D + S (total)
 Bearing : Support 1 - LC #2 = D + S
 Support 2 - LC #2 = D + S

D=dead S=snow

All LC's are listed in the Analysis output

Load Patterns: s=S/2, X=L+S or L+Lr, _=no pattern load in this span

Load combinations: ASD Basic from ASCE 7-16 2.4

CALCULATIONS:

V max = 7040, V design = 5977 (NDS 3.4.3.1(a)) lbs; M(+) = 28160 lbs-ft

EI = 2029.78e06 lb-in²

"Live" deflection is due to all non-dead loads (live, wind, snow...)

Total deflection = 1.00 permanent + "live"

Design Notes:

1. Analysis and design are in accordance with the ICC International Building Code (IBC 2021) and the National Design Specification (NDS 2018), using Allowable Stress Design (ASD). Design values are from the NDS Supplement.
2. Please verify that the default deflection limits are appropriate for your application.
3. Glulam design values are for materials conforming to ANSI 117-2015 and manufactured in accordance with ANSI A190.1-2012
4. GLULAM: bxd = actual breadth x actual depth.
5. Glulam Beams shall be laterally supported according to the provisions of NDS Clause 3.3.3.
6. GLULAM: bearing length based on smaller of Fcp(tension), Fcp(comp'n).



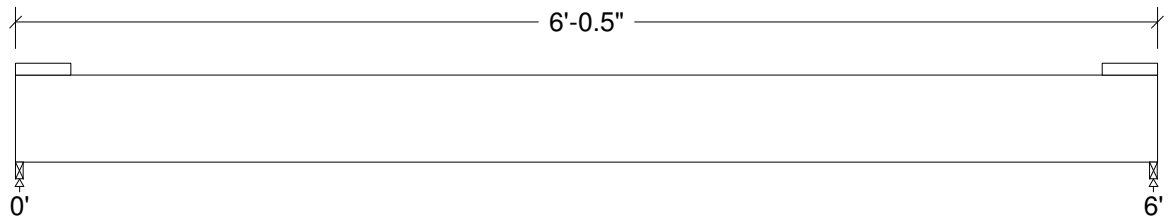
7448 W Mercer Island
Mercer Island, WA 98040
1_6 Header
Apr. 23, 2025 15:32

Design Check Calculation Sheet WoodWorks Sizer 2023

Loads:

| Load | Type | Distribution | Pat- tern | Location [ft] | | Magnitude | | Unit |
|------|------|--------------|--------------|---------------|-----|-----------|-----|------|
| | | | | Start | End | Start | End | |
| DL | Dead | Full UDL | | | | 30.0 | | plf |
| SL | Snow | Full UDL | | | | 50.0 | | plf |

Maximum Reactions (lbs), Bearing Capacities (lbs) and Bearing Lengths (in) :



| | | | |
|-------------|-------|--|-------|
| Unfactored: | | | |
| Dead | 91 | | 91 |
| Snow | 151 | | 151 |
| Factored: | | | |
| Total | 242 | | 242 |
| Bearing: | | | |
| Capacity | | | |
| Beam | 1094 | | 1094 |
| Support | 1211 | | 1211 |
| Des ratio | | | |
| Beam | 0.22 | | 0.22 |
| Support | 0.20 | | 0.20 |
| Load comb | #2 | | #2 |
| Length | 0.50* | | 0.50* |
| Min req'd | 0.50* | | 0.50* |
| Cb | 1.00 | | 1.00 |
| Cb min | 1.00 | | 1.00 |
| Cb support | 1.11 | | 1.11 |
| Fcp sup | 625 | | 625 |

*Minimum bearing length setting used: 1/2" for end supports

Lumber-soft, D.Fir-L (N), No.1/No.2, 4x6 (3-1/2"x5-1/2")

Supports: All - Timber-soft Beam, D.Fir-L (N) No.2
Total length: 6'-0.5"; Clear span: 5'-11.5"; Volume = 0.8 cu.ft.
Lateral support: top = at supports, bottom = at supports;
This section PASSES the design code check.

Analysis vs. Allowable Stress and Deflection using NDS 2018 :

| Criterion | Analysis Value | Design Value | Unit | Analysis/Design |
|--------------|------------------|----------------|------|-------------------|
| Shear | $f_v = 16$ | $F_v' = 207$ | psi | $f_v/F_v' = 0.08$ |
| Bending (+) | $f_b = 245$ | $F_b' = 1271$ | psi | $f_b/F_b' = 0.19$ |
| Live Defl'n | $0.02 = < L/999$ | $0.20 = L/360$ | in | 0.09 |
| Total Defl'n | $0.03 = < L/999$ | $0.40 = L/180$ | in | 0.08 |

Additional Data:

| FACTORS: | F/E(psi) | CD | CM | Ct | CL | CF | Cfu | Cr | Cfrt | Ci | LC# |
|----------|-------------|------|------|------|-------|-------|-----|------|------|------|-----|
| Fv' | 180 | 1.15 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 2 |
| Fb'+ | 850 | 1.15 | 1.00 | 1.00 | 1.000 | 1.300 | - | 1.00 | 1.00 | 1.00 | 2 |
| Fcp' | 625 | - | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | - |
| E' | 1.6 million | | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 2 |

CRITICAL LOAD COMBINATIONS:

Shear : LC #2 = D + S

Bending(+): LC #2 = D + S

Deflection: LC #2 = D + S (live)

LC #2 = D + S (total)

Bearing : Support 1 - LC #2 = D + S

Support 2 - LC #2 = D + S

D=dead S=snow

All LC's are listed in the Analysis output

Load Patterns: s=S/2, X=L+S or L+Lr, _=no pattern load in this span

Load combinations: ASD Basic from ASCE 7-16 2.4

CALCULATIONS:

V max = 240, V design = 202 (NDS 3.4.3.1(a)) lbs; M(+) = 360 lbs-ft

EI = 77.64e06 lb-in²

"Live" deflection is due to all non-dead loads (live, wind, snow...)

Total deflection = 1.00 permanent + "live"

Design Notes:

1. Analysis and design are in accordance with the ICC International Building Code (IBC 2021) and the National Design Specification (NDS 2018), using Allowable Stress Design (ASD). Design values are from the NDS Supplement.
2. Please verify that the default deflection limits are appropriate for your application.
3. Sawn lumber bending members shall be laterally supported according to the provisions of NDS Clause 4.4.1.



7448 W Mercer Island
Mercer Island, WA 98040
1_6 Header
Apr. 23, 2025 15:44

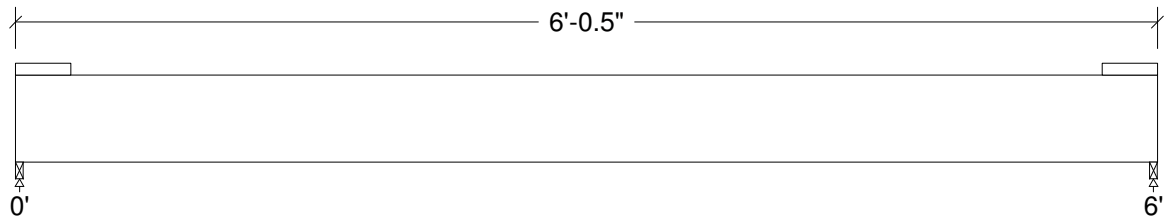
Design Check Calculation Sheet

WoodWorks Sizer 2023

Loads:

| Load | Type | Distribution | Pat- tern | Location [ft] | | Magnitude | | Unit |
|------|------|--------------|--------------|---------------|-----|-----------|-----|------|
| | | | | Start | End | Start | End | |
| DL | Dead | Full UDL | | | | 30.0 | | plf |
| SL | Snow | Full UDL | | | | 50.0 | | plf |

Maximum Reactions (lbs), Bearing Capacities (lbs) and Bearing Lengths (in) :



| | | | |
|-------------|-------|--|-------|
| Unfactored: | | | |
| Dead | 91 | | 91 |
| Snow | 151 | | 151 |
| Factored: | | | |
| Total | 242 | | 242 |
| Bearing: | | | |
| Capacity | | | |
| Beam | 1094 | | 1094 |
| Support | 1211 | | 1211 |
| Des ratio | | | |
| Beam | 0.22 | | 0.22 |
| Support | 0.20 | | 0.20 |
| Load comb | #2 | | #2 |
| Length | 0.50* | | 0.50* |
| Min req'd | 0.50* | | 0.50* |
| Cb | 1.00 | | 1.00 |
| Cb min | 1.00 | | 1.00 |
| Cb support | 1.11 | | 1.11 |
| Fcp sup | 625 | | 625 |

*Minimum bearing length setting used: 1/2" for end supports

Lumber-soft, D.Fir-L (N), No.1/No.2, 4x6 (3-1/2"x5-1/2")

Supports: All - Timber-soft Beam, D.Fir-L (N) No.2
Total length: 6'-0.5"; Clear span: 5'-11.5"; Volume = 0.8 cu.ft.
Lateral support: top = at supports, bottom = at supports;
This section PASSES the design code check.

Analysis vs. Allowable Stress and Deflection using NDS 2018 :

| Criterion | Analysis Value | Design Value | Unit | Analysis/Design |
|--------------|------------------|----------------|------|-------------------|
| Shear | $f_v = 16$ | $F_v' = 207$ | psi | $f_v/F_v' = 0.08$ |
| Bending (+) | $f_b = 245$ | $F_b' = 1271$ | psi | $f_b/F_b' = 0.19$ |
| Live Defl'n | $0.02 = < L/999$ | $0.20 = L/360$ | in | 0.09 |
| Total Defl'n | $0.03 = < L/999$ | $0.40 = L/180$ | in | 0.08 |

Additional Data:

| FACTORS: | F/E(psi) | CD | CM | Ct | CL | CF | Cfu | Cr | Cfrt | Ci | LC# |
|----------|-------------|------|------|------|-------|-------|-----|------|------|------|-----|
| Fv' | 180 | 1.15 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 2 |
| Fb'+ | 850 | 1.15 | 1.00 | 1.00 | 1.000 | 1.300 | - | 1.00 | 1.00 | 1.00 | 2 |
| Fcp' | 625 | - | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | - |
| E' | 1.6 million | | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 2 |

CRITICAL LOAD COMBINATIONS:

Shear : LC #2 = D + S

Bending(+): LC #2 = D + S

Deflection: LC #2 = D + S (live)

LC #2 = D + S (total)

Bearing : Support 1 - LC #2 = D + S

Support 2 - LC #2 = D + S

D=dead S=snow

All LC's are listed in the Analysis output

Load Patterns: s=S/2, X=L+S or L+Lr, _=no pattern load in this span

Load combinations: ASD Basic from ASCE 7-16 2.4

CALCULATIONS:

V max = 240, V design = 202 (NDS 3.4.3.1(a)) lbs; M(+) = 360 lbs-ft

EI = 77.64e06 lb-in²

"Live" deflection is due to all non-dead loads (live, wind, snow...)

Total deflection = 1.00 permanent + "live"

Design Notes:

1. Analysis and design are in accordance with the ICC International Building Code (IBC 2021) and the National Design Specification (NDS 2018), using Allowable Stress Design (ASD). Design values are from the NDS Supplement.
2. Please verify that the default deflection limits are appropriate for your application.
3. Sawn lumber bending members shall be laterally supported according to the provisions of NDS Clause 4.4.1.



7448 W Mercer Island
Mercer Island, WA 98040
2_1 Floor Joist
Apr. 23, 2025 15:44

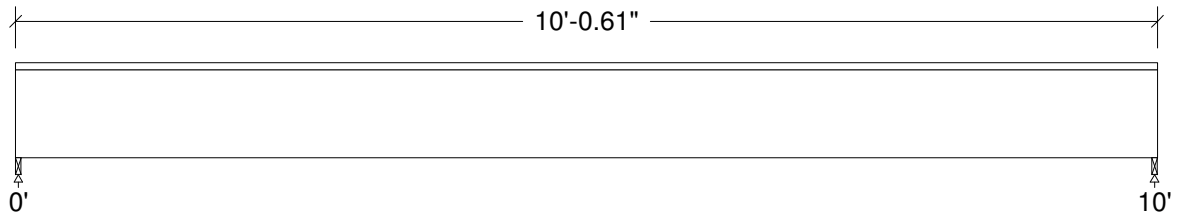
Design Check Calculation Sheet

WoodWorks Sizer 2023

Loads:

| Load | Type | Distribution | Pat-tern | Location [ft] | | Magnitude | | Unit |
|------|------|--------------|----------|---------------|-----|-----------|---------|------|
| | | | | Start | End | Start | End | |
| DL | Dead | Full Area | | | | 15.00 | (16.0") | psf |
| LL | Live | Full Area | | | | 40.00 | (16.0") | psf |

Maximum Reactions (lbs), Bearing Capacities (lbs) and Bearing Lengths (in) :



| | | | |
|-------------|------|--|------|
| Unfactored: | | | |
| Dead | 101 | | 101 |
| Live | 268 | | 268 |
| Factored: | | | |
| Total | 369 | | 369 |
| Bearing: | | | |
| Capacity | | | |
| Joist | 369 | | 369 |
| Support | 711 | | 711 |
| Des ratio | | | |
| Joist | 1.00 | | 1.00 |
| Support | 0.52 | | 0.52 |
| Load comb | #2 | | #2 |
| Length | 0.61 | | 0.61 |
| Min req'd | 0.61 | | 0.61 |
| Cb | 1.00 | | 1.00 |
| Cb min | 1.00 | | 1.00 |
| Cb support | 1.25 | | 1.25 |
| Fcp sup | 625 | | 625 |

Lumber-soft, Hem-Fir (N), No.1/No.2, 2x10 (1-1/2"x9-1/4")

Supports: All - Timber-soft Beam, D.Fir-L (N) No.2

Floor joist spaced at 16.0" c/c; Total length: 10'-0.63"; Clear span: 9'-11.38"; Volume = 1.0 cu.ft.

Lateral support: top = continuous, bottom = at supports; Repetitive factor: applied where permitted (refer to online help);

This section PASSES the design code check.

Analysis vs. Allowable Stress and Deflection using NDS 2018 :

| Criterion | Analysis Value | Design Value | Unit | Analysis/Design |
|--------------|------------------|----------------|------|-------------------|
| Shear | $f_v = 33$ | $F_v' = 145$ | psi | $f_v/F_v' = 0.23$ |
| Bending (+) | $f_b = 514$ | $F_b' = 1265$ | psi | $f_b/F_b' = 0.41$ |
| Live Defl'n | $0.08 = < L/999$ | $0.33 = L/360$ | in | 0.23 |
| Total Defl'n | $0.09 = < L/999$ | $0.50 = L/240$ | in | 0.18 |

Additional Data:

| FACTORS: | F/E (psi) | CD | CM | Ct | CL | CF | Cfu | Cr | Cfrt | Ci | LC# |
|----------|--------------|------|------|------|-------|-------|-----|------|------|------|-----|
| Fv' | 145 | 1.00 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 2 |
| Fb'+ | 1000 | 1.00 | 1.00 | 1.00 | 1.000 | 1.100 | - | 1.15 | 1.00 | 1.00 | 2 |
| Fcp' | 405 | - | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | - |
| E' | 1.6 million | 1.00 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 2 |
| Emin' | 0.58 million | 1.00 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 2 |

CRITICAL LOAD COMBINATIONS:

Shear : LC #2 = D + L
 Bending (+): LC #2 = D + L
 Deflection: LC #2 = 0.5D + L (live)
 LC #2 = 0.5D + L (total)
 Bearing : Support 1 - LC #2 = D + L
 Support 2 - LC #2 = D + L

D=dead L=live

All LC's are listed in the Analysis output

Load combinations: ASD Basic from ASCE 7-16 2.4

CALCULATIONS:

V max = 367, V design = 308 (NDS 3.4.3.1(a)) lbs; M(+) = 917 lbs-ft

EI = 158.29e06 lb-in²

"Live" deflection is due to all non-dead loads (live, wind, snow...)

Total deflection = 0.50 permanent + "live"

Design Notes:

1. Analysis and design are in accordance with the ICC International Building Code (IBC 2021) and the National Design Specification (NDS 2018), using Allowable Stress Design (ASD). Design values are from the NDS Supplement.
2. Please verify that the default deflection limits are appropriate for your application.
3. Sawn lumber bending members shall be laterally supported according to the provisions of NDS Clause 4.4.1.



7448 W Mercer Island
Mercer Island, WA 98040
2_2 Beam
Apr. 23, 2025 15:48

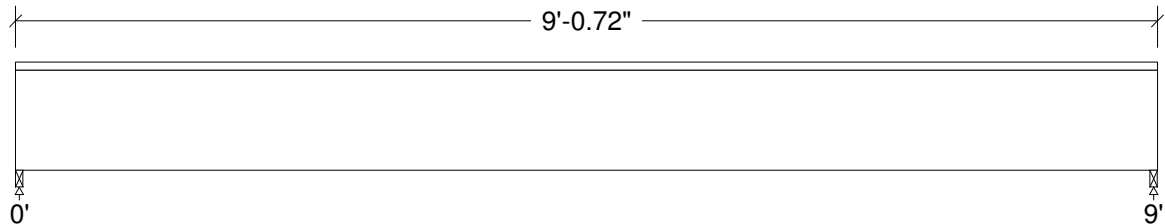
Design Check Calculation Sheet

WoodWorks Sizer 2023

Loads:

| Load | Type | Distribution | Pat-tern | Location [ft] | | Magnitude | | Unit |
|------|------|--------------|----------|---------------|-----|-----------|-----|------|
| | | | | Start | End | Start | End | |
| DL | Dead | Full UDL | | | | 150.0 | | plf |
| LL | Live | Full UDL | | | | 400.0 | | plf |

Maximum Reactions (lbs), Bearing Capacities (lbs) and Bearing Lengths (in) :



| | | | |
|-------------|------|--|------|
| Unfactored: | | | |
| Dead | 680 | | 680 |
| Live | 1812 | | 1812 |
| Factored: | | | |
| Total | 2492 | | 2492 |
| Bearing: | | | |
| Capacity | | | |
| Beam | 2492 | | 2492 |
| Support | 2661 | | 2661 |
| Des ratio | | | |
| Beam | 1.00 | | 1.00 |
| Support | 0.94 | | 0.94 |
| Load comb | #2 | | #2 |
| Length | 0.72 | | 0.72 |
| Min req'd | 0.72 | | 0.72 |
| Cb | 1.00 | | 1.00 |
| Cb min | 1.00 | | 1.00 |
| Cb support | 1.07 | | 1.07 |
| Fcp sup | 625 | | 625 |

Timber-soft, D.Fir-L (N), No.2, 6x10 (5-1/2"x9-1/2")

Supports: All - Timber-soft Beam, D.Fir-L (N) No.2
Total length: 9'-0.75"; Clear span: 8'-11.25"; Volume = 3.3 cu.ft.; Beam or stringer
Lateral support: top = continuous, bottom = at supports;
This section PASSES the design code check.

Analysis vs. Allowable Stress and Deflection using NDS 2018 :

| Criterion | Analysis Value | Design Value | Unit | Analysis/Design |
|--------------|----------------|----------------|------|-------------------|
| Shear | $f_v = 58$ | $F_v' = 170$ | psi | $f_v/F_v' = 0.34$ |
| Bending (+) | $f_b = 808$ | $F_b' = 875$ | psi | $f_b/F_b' = 0.92$ |
| Live Defl'n | $0.12 = L/934$ | $0.30 = L/360$ | in | 0.39 |
| Total Defl'n | $0.14 = L/786$ | $0.60 = L/180$ | in | 0.23 |

Additional Data:

| FACTORS: | F/E(psi) | CD | CM | Ct | CL | CF | Cfu | Cr | Cfrt | Ci | LC# |
|----------|-------------|------|------|------|-------|-------|-----|------|------|------|-----|
| Fv' | 170 | 1.00 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 2 |
| Fb'+ | 875 | 1.00 | 1.00 | 1.00 | 1.000 | 1.000 | - | 1.00 | 1.00 | 1.00 | 2 |
| Fcp' | 625 | - | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | - |
| E' | 1.3 million | 1.00 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 2 |

CRITICAL LOAD COMBINATIONS:

Shear : LC #2 = D + L

Bending(+): LC #2 = D + L

Deflection: LC #2 = 0.5D + L (live)

LC #2 = 0.5D + L (total)

Bearing : Support 1 - LC #2 = D + L

Support 2 - LC #2 = D + L

D=dead L=live

All LC's are listed in the Analysis output

Load Patterns: s=S/2, X=L+S or L+Lr, _=no pattern load in this span

Load combinations: ASD Basic from ASCE 7-16 2.4

CALCULATIONS:

V max = 2475, V design = 2023 (NDS 3.4.3.1(a)) lbs; M(+) = 5569 lbs-ft

EI = 510.84e06 lb-in²

"Live" deflection is due to all non-dead loads (live, wind, snow...)

Total deflection = 0.50 permanent + "live"

Design Notes:

1. Analysis and design are in accordance with the ICC International Building Code (IBC 2021) and the National Design Specification (NDS 2018), using Allowable Stress Design (ASD). Design values are from the NDS Supplement.
2. Please verify that the default deflection limits are appropriate for your application.
3. Sawn lumber bending members shall be laterally supported according to the provisions of NDS Clause 4.4.1.